Design of experiments for determining the parameters affecting the behavior of the wheat straw adsorbent of hydrocarbons dispensed in water

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Abstract

Wheat straw, a lignocellulosic matter, with content up to 20% lignin on dry basis has been found to be an efficient adsorbent of hydrocarbons in water. In the present study the hydrocarbon absorptive capability of wheat straw that was previously treated with acid is investigated in oil spills which were created in the laboratory by dispersing diesel and crude oil in water. A 3-level Box–Behnken design of experiments has been executed in order to determine the parameters affecting the behavior of the acid-hydrolyzed wheat straw as an adsorbent, with design factors the maleic acid (MC4H4O4) concentration, and hydrolysis parameters temperature and reaction time. The absorbency of wheat straw is appraised by a combination of analytical methods such as Mercury Porosimetry (MP), Thermogravinetric Analysis (TGA), Total Organic Carbon (TOC) and Scanning Electron Microscope (SEM).

Keywords: wheat straw, oils spills, TGA, SEM, TOC, porosimetry.

1 Introduction

Spilled oil provokes severe environmental damages. The major problem with contaminated water is that it could not be used into municipal water supply either in industry or in agriculture [1]. The public concern for a healthy environment has led to new improved techniques and methods in order to deal with hazardous



materials. In an effort to devise new methods for containment/mitigation of oil spills, we experimented with agricultural waste such as wheat straw, which is inexpensive, and readily available, low oil sorption capacity as well as low hydrophobicity [2].

Hydrocarbons are organic compounds of hydrogen and carbon, of different composition and chemical structure, classified in various groups, aromatic, alkanes, alkenes, cycloalkanes and alkynes. Most hydrocarbons are present in crude oil, where decomposed organic matter provides an abundance of carbon and hydrogen which can be bonded in various ways. Oil is one of the major resources of energy and commodity chemicals in the industrialized world at present. Chemical dispersion, in situ burning, mechanical containment and oil sorption by adsorbents are generally accepted clean-up methods to combat oil pollution [3].

In the present work, wheat straw, a lignocellulosic material, is studied for its use as an adsorbent of hydrocarbons in water [4]. Studies show that the surface energy of a lignin film is similar to that of cellulose, but the contact angle of water for lignin is higher than that for cellulose, i.e., lignin is more hydrophobic or less hydrophilic than cellulose. The lignin surface contains charged functional groups that may attract charged oil droplets.

Straw-like adsorbing materials are capable of holding oil as a result of two processes: adsorption and absorption. Wax coverage making the straw surface hydrophobic and capillary forces determine the efficiency of oil removal. The adsorption capacity depends primarily on the chemical structure of straw tissue that is in direct contact with oil and is a function of structure of straw stalks in bundles, distances between stalks, and cross-sections of each stalk and leaf. Due to high oil adsorption by straw, oil is mostly held by capillary forces on straw tissue and interior parts of stalk and by oil bridges between stalks. As a result, absorption of oil depends on the surface properties of straw.

In the present work, thermo-hydrolyzed wheat straw treated with maleic acid has been examined as hydrocarbon adsorbent. The efficiency of wheat straw as adsorbent is determined via several analytical methods, including TGA, TOC, SEM, and MP.

A 3-level Box–Behnken design was chosen, with three center points to check for curvature in the response surface. This is a type of response surface design that does not contain an embedded factorial or fractional factorial design. Box–Behnken designs have treatment combinations that are at the midpoints of the edges of the experimental space and require at least three factors. Factors can be categorical or arithmetic variables and can assume a limited number of possible values, known as factor levels, and are controlled in the experiment [5]. The factors and their levels chosen for this experiment are displayed in Table 1.

A Design of Experiments (DOE) approach was conducted in order to examine the effects of experimental conditions on the pH and Solid Residue Yield (SRY) of 15 samples. Those samples were examined for 5 different absorption environments such as crude oil, diesel, crude oil spill, diesel spill as well as water. Table 2 below presents all the results of the performed analytical methods of the treated wheat straw. Sample 5, after hydrolysis with Maleic acid 0.01M, in 160°C at 0 min, showed the best performance in all the performed analytical methods.

Factors	Fa	Unite		
raciois	-1	0	1	Units
MC ₄ H ₄ O ₄ Concentration, MC	0.01	0.05	0.09	М
Temperature, Temp	140	160	180	°C
Reaction time, t	0	25	50	min

 Table 1:
 DOE critical factor and their levels.

Table 2: DOE table, experimental samples and results (porosity, TOC and TGA).

Sample	мс	Temp	t	Weight	porosity	Tot. spec. surface area (m²/g)	Bulk Density (g/cm3)	тос (%)	TGA	Peak Temp.
1	0.09	140	25	4.20	77.844	13.347	0.266	29.19	72.65	320.73
2	0.01	160	50	4.20	75.211	22.053	0.307	28.45	67.93	360.27
3	0.09	180	25	4.05	67.755	17.814	0.342	24.12	65.50	312.60
4	0.09	160	0	4.02	70.642	21.899	0.289	27.73	72.73	301.73
5	0.01	160	0	4.30	76.748	32.500	0.317	41.43	87.35	349.04
6	0.09	160	50	4.00	73.543	22.186	0.282	25.24	73.02	360.75
7	0.05	180	0	4.18	71.57	19.122	0.317	25.98	73.27	318.45
8	0.01	180	25	4.10	68.512	18.227	0.377	26.56	71.39	340.46
9	0.05	140	50	4.10	78.784	22.263	0.257	29.43	74.70	356.29
10	0.05	160	25	4.18	74.597	21.752	0.311	28.23	76.47	369.43
11	0.05	180	50	4.10	70.948	17.379	0.361	23.06	71.95	344.38
12	0.01	140	25	4.09	74.44	30.821	0.299	40.13	76.60	345.49
13	0.05	160	25	4.18	73.832	20.246	0.274	36.34	71.06	315.38
14	0.05	160	25	4.19	76.525	20.360	0.293	28.99	76.47	369.43
15	0.05	140	0	3.80	81.158	25.622	0.260	28.22	75.43	356.61

2 Materials and methods

2.1 Wheat straw treatment method

The material used was the wheat straw which was harvested in 2012, at the Kapareli village near the city of Thiva in the area of Kopaida in central Greece [6]. The acid hydrolysis process took place in a 3.75L batch PARR 4843. The optimum conditions for the hydrolysis process were presented in Table 1. The acid hydrolysis process performed at a liquid-to-solid radio of 20:1, which resulted in a 100g of wheat straw added to a 2000ml volume of liquid [7].

2.2 Modified wheat straw oil absorbance method

In the modified wheat straw oil absorbance method, the ratio of water or oil absorbed to dry adsorbent weight was based on the ASTM F726-06 method. Following the standard method, 10PPM diesel produced by Hellenic Petroleum SA as well as crude oil was used.



2.3 Wheat straw analysis methods

In previous studies, untreated and auto-hydrolyzed wheat straw were examined as hydrocarbon adsorbents with the use of several analytical method, such as MP, TGA, TOC, Fourier Transform Infrared Spectrometry (FTIR), X-Ray Diffraction Analysis (XRD), SEM, and Atomic Absorption Spectrometry (AAS). The first four were proved to be the most important for the following straw evaluation performance analysis [8].

2.3.1 Total Organic Carbon (TOC)

The treated, dried and milled wheat straw is mounted on metal stubs and is heated to 105° C in order to remove the moisture. The sample is placed in a crucible which is heated to 550° C for 2 hours [10]. The carbon content (% C) was calculated from the ash content (% ash) using the following equation [11]:

$$%C = ((100 - \%ash) * 100) / 1.8$$
 (1)

2.3.2 Mercury porosimetry

An idea of the adsorptive capacity of the modified wheat straw samples can be obtained with mercury porosimetry which detects meso- and macro-pore sizes $(2nm-100\mu m)$. Measurements were obtained using a Pascal 440 Porosimeter (Thermo Electron). Pressures between 0.01Torr and 200MPa can be developed which allows pores of 100 μm to 3.75nm radius to be measured. In order to obtain reproducible results, it was necessary to obtain good vacuum before filling the sample cell with mercury at 0.01Torr for 30min [9].

2.3.3 Thermogravimetric Analysis (TGA)

Thermogravimetric measurements were performed with a Mettler-Toledo TGA/DSC 1 HT Integrated Thermal Gravimetric Analyzer with high-purity nitrogen as a carrier gas and a flow rate of 40mL/min. About 5–12mg samples were placed in an alumina pan of 70µL each time. The samples were heated from room temperature to 800° C at a heating rate of 10° C/min. The calculated thermogravimetic rate data were automatically recorded by the Integrated Thermal Gravimetric Analyzer system of Mettler-Toledo, using a STARe Thermal Analysis Software. The thermogravimetric experiment was used to obtain the parameters of chemical dynamics and the influence of any error was reduced as much as possible. The average size of all samples was below 0.5mm, so that the weight loss of the samples was controlled by reaction kinetics.

2.3.4 Scanning Electron Microscopy (SEM)

The morphology of the treated wheat straw fibers was determined from dried and milled samples, mounted on metal stubs, using a scanning electron microscope (SEM). Images were taken at 30kV by a FEI Quanta 200 microscope, with a LFD detector and magnifications that ranged from 300 to 4000.



3 Results and discussion

3.1 Modified wheat straw analysis after oil absorbance measurements

The analysis of raw modified wheat straw samples showed that some treatment combinations produced best results and these are considered as most appropriate to focus on for oil absorbance measurements. For example, attention can be drawn by samples 5 and 12 for further analysis (Table 2).

3.1.1 Total Organic Carbon (TOC) results

Table 3 shows the TOC content in acid hydrolysed wheat straw after exposure in different adsorbent environments such as crude oil, oil spill crude and diesel, diesel as well as water. More specifically, sample 5 with hydrolysis conditions maleic acid 0.01M, 160°C temperature and 0 minutes reaction time, show the highest TOC percentage. Moreover, sample 13 which is exposed to maleic acid at medium concentration (0.05M), resulted in 20.95% and 26.14% TOC.

					Oil		Oi1	
				Crude	spill		spill	
Sample	MC	Temp	t	oil	diesel	Diese1	Crude	Water
1	0.09	140	25	11.35	14.37	15.13	14.18	6.65
2	0.01	160	50	10.05	14.24	12.51	13.01	6.92
3	0.09	180	25	3.11	8.26	7.20	7.73	0.18
4	0.09	160	0	3.34	12.77	11.53	13.29	5.30
5	0.01	160	0	31.64	35.21	31.08	34.27	28.50
6	0.09	160	50	3.32	10.46	5.82	6.27	1.67
7	0.05	180	0	4.12	8.03	8.52	7.85	1.05
8	0.01	180	25	4.67	9.73	6.64	6.43	1.93
9	0.05	140	50	11.94	20.9	19.92	18.23	6.83
10	0.05	160	25	7.92	14.13	9.81	11.78	5.00
11	0.05	180	50	0.83	0.99	1.90	1.34	0.47
12	0.01	140	25	29.74	32.52	31.61	30.96	28.45
13	0.05	140	0	24.32	26.16	24.56	25.32	20.95

Table 3: TOC results after hydrocarbon absorbence.

Acid hydrolyzed wheat straw in oil spills of crude and diesel presents better results regarding TOC reduction (Figure 1). The initial TOC content in untreated wheat straw, which has been tested in previous study, was 51.7% [8]. Based on the current results, it should emphasized that TOC reduction is gradual, starting with acid-hydrolysed wheat straw as raw material and following with the samples after the absorbance of hydrocarbons.

3.1.2 Mercury porosimetry results

Figure 2 depicts the reduction of mercury porosimetry for modified wheat straw in sample 5 after five different kinds of hydrocarbon absorbents. The total porosity ranges from 19.49 to 73.41%, according to the adsorbent conditions. The most important factor of those results is the reduction of % porosimetry between the measurements before and after adsorption which was calculated between 57.25



Figure 1: TOC average after hydrocarbon absorbency.



Figure 2: Reduction of % adsorbent porosity before and after absorbance.

and 3.34%. The maximum porosimetry reduction is presented in crude oil as well as in oil spill crude oil, 57.25 and 45.47% respectively. It is worth highlighting that high porosimetry reduction is presented after the absorbance of oil spill diesel. Based on Table 4 it is assumed that the pore radius distribution varies significantly according to the mean that the adsorption took place. This fact depends on the size of the molecules that have been adsorbed from the adsorbent material indicating its selectivity. For instance it is obvious that the material shows selectivity to lighter hydrocarbons with small size molecules therefore the free pores that their radius is measured are the bigger ones.



MC	Temp	Т	Weight (g)	% porosity	Average pore radius (micron)	Apparent density (g/cm²)	тос	TOC abs.	Pore reduction
0.01	160	0	4.30	76.75	0.483	1.36	41.43		
0.01	160	0	Crude oil	19.50	0.2112	1.01	41.43	31.64	57.25
0.01	160	0	Oi1 spi11 diese1	37.81	3.502	0.97	41.43	35.21	38.94
0.01	160	0	Diese1	54.44	0.994	1.08	41.43	31.08	22.31
0.01	160	0	Oi1 spi11 crude	31.28	4.567	0.99	41.43	34.27	45.47
0.01	160	0	water	73.41	0.508	1.24	41.43	28.50	3.34

Table 4: Porosity and TOC results after hydrocarbons and water absorbance.

3.1.3 Thermogravimetric analysis (TGA)

The pyrolysis profiles, in particular, demonstrate an increase in decomposition temperature onset temperature. peak and maximum rate of decomposition, indicative of a lower reactivity. The profiles are typical of lignocellulosic materials, showing the onset of an initial volatilization stage around 220°C followed by a char oxidation stage at higher temperatures. Sample 5 before the adsorption shows a mass loss of 87% in two stages. The first stage is at 350°C beginning at 250°C and indicating the decomposition of cellulose and hemicellulose. The second stage at 500°C is related to the decomposition of lignin. In case of adsorption of crude oil there is a significant increase in the total mass loss indicating the adsorption of crude oil. The great loss is shown at 350°C indicating the removal of cellulose and hemicellulose and heavy crude oil fractions. The mass loss begins from significant low temperatures around 80°C indicating the removal of lighter fractions under C5 such as naptha. Moreover there is a slight weight loss at 420°C indicating the removal of very heavy fractions >C15. The creation of chemical bonds between lignin and hydrocarbons enhance the lignin removal in lower temperatures. In case of diesel spill the mass loss starts at 70°C with light diesel fractions and maximizes at 350°C indicating the removal of cellulose, hemicellulose and heavy diesel fractions (C13). The adsorption in water matter increases the decomposition temperature of the treated straw (sample 13). This depends on the partial dilution of cellulose and hemicellulose in water that is trapped in a hydrophobic lignin base matrix that deteriorates the removal of sensitive thermo-degradable matter.

3.1.4 Scanning Electron Microscopy (SEM)

SEM images of hydrothermally pretreated in acidic environment wheat straw were obtained. In our previous study of untreated wheat straw, the straw is surrounded by a sheath leaf and at slightly higher magnification the individual cells of the straw wall can be identified. A high-resolution scan (of a primary cell wall lining the straw cavity shows interwoven cellulose microfibrils, partially imbedded in non-cellulosic polymers. In hydrothermally pretreated wheat straw, the defibrillating effect of the pretreatment causes the individual fibers to partially separate, as can be seen in SEM images. The pretreatment leaves a surface layer of debris and re-deposited cell-wall polymers on the individual fibers.





Figure 3: TGA results of sample 5.

The overall structure of the individual fibers seems to show large structural changes such as rupture of fibers or a visible increase of porosity, which are believed to be associated with thermal pretreatments. As it is observed in Figure 4 the differences between water and spill oils are clear. Holes and cracks were seen in the fibers indicating that the accessibility of the internal parts of the cell wall matrix had been improved due to structural dislocations. The primary and secondary cell walls appeared to be fully intact, except for the pits and simple perforations that already exist in certain cell types. Consequently, the effectiveness of pretreatment must be related to hemicellulose removal and lignin relocation. This is in spite of the fact that lignin is not removed by the pretreatment and that lignin is known to be responsible for hydrocarbon adsorbance.



Figure 4: SEM results of sample 5.



4 Conclusions

Lignocellulosic materials are superior to non-porous materials with regards to surface area. This advantage sets them as good candidates for sorption material. The oil absorptivity is based on interaction forces of Van der Walls type between oil and wheat straw. The sorption is based on the fact that both oil and wax are hydrocarbons, a fact that explains the physical interaction of oil through its irregular surface morphology [2]. Previous studies have shown that natural sorbents could be sufficiently used for oils spills removal more so than polypropylene materials that were used more often at the time [12]. This can be better explained by a combination of porosimetry results as well as TOC reduction. High porosity values which are shown to form the specimen of 0.01M Maleic acid, 160°C temperatures and 0 min reaction time, correspond to maximum TOC. Likewise, average porosimetry reduction after both acid hydrolysis and hydrocarbon adsorbents corresponds to average TOC reduction. Therefore, it is obvious that through acid hydrolysis we achieve high reduction of average porosimetry and TOC in wheat straw which has adsorbed crude oil and oil spills. This is also confirmed by SEM results.

Acknowledgements

This research has been co-financed by the European Union (European Social Fund – ESF) and Greek national funds through the Operational Program "Education and Lifelong Learning" of the National Strategic Reference Framework (NSRF). Research Funding Program: THALES. Investing in knowledge society through the European Social Fund. Project: THALIS – University Of Piraeus – Development of New Material from Waste Biomass for Hydrocarbons Adsorption in Aquatic Environments.

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