# COST EFFECTIVE MARINE EXHAUST ABATEMENT FOR NOx, SOx AND SOOT

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#### ABSTRACT

This paper bridges controversy surrounding marine open loop exhaust gas scrubbing restrictions. The solutions offered in this paper apply equally well to both open and closed loop scrubbing methodology. The chlorine dioxide (ClO<sub>2</sub>) based gas/mist scrubbing technology presented in this paper works equally well in open and closed loop applications. This ClO<sub>2</sub> based gas/mist phase exhaust scrubbing technology effectively removes more than 99% of SO<sub>X</sub> and most of the organic compounds including polycyclic aromatic hydrocarbon compounds (PAH) that create soot in marine exhaust. The very same ClO<sub>2</sub> based gas/mist scrubbing equipment can also be configured to simultaneously treat SO<sub>X</sub> and NO<sub>X</sub>, plus most of the organic compounds that create soot. Where permitted, the sulfur based salts generated from the ClO<sub>2</sub> based gas/mist SO<sub>X</sub> abatement process can be discharged directly into the sea without the typical additional washwater treatment required when SO<sub>X</sub> is treated with seawater scrubbers. Alternatively, when closed loop scrubbing is required, this ClO<sub>2</sub> based gas/mist scrubbing process can store the sulfur based SO<sub>X</sub> reaction products as a very low volume paste until the ship is in a location that allows paste to be discharged into the sea. The scrubbing device is a simple cylinder that fits into the ship's funnel and a small skid of equipment plus chemical storage that can be configured together or separately in the mechanical area of the ship. Overall, this equipment has a small physical size, high removal efficiency, and low equipment/operating cost. This ClO<sub>2</sub> based gas/mist phase scrubbing technology can be combined with existing abatement equipment or used on its own. The ClO<sub>2</sub> based gas/mist scrubbing technology is in full compliance with IMO regulations for SOx, NOx and soot.

Keywords: exhaust, scrubber, open-loop, closed-loop, chlorine dioxide, SOx, NOx, soot.

## 1 INTRODUCTION

The ClO<sub>2</sub> based marine exhaust gas treatment process has 6 distinct features:

- The SO<sub>X</sub> scrubbing byproducts from this ClO<sub>2</sub> based gas/mist scrubbing method can be discharged directly into the sea. It does not require the secondary washwater treatment used when SO<sub>X</sub> is scrubbed with seawater.
- When a ship is operated in a zone that requires closed loop SO<sub>X</sub> scrubbing, the sulfur based salts and treated soot precursors can be temporarily stored as low volume paste until the vessel reaches an area that authorizes discharge of the sulfur based salt paste into the sea.
- Where required, this very same equipment can treat SOx, and NOx and some organics that are soot precursors. The change only requires a variation in the ClO<sub>2</sub> dosing rate.
- NO<sub>X</sub> scrubbing byproducts are stored as low volume paste that is separate from SO<sub>X</sub> scrubbing byproducts with very low cross contamination levels.
- The generation of paste from SO<sub>X</sub> or NO<sub>X</sub> scrubbing is done with a low energy process that recycles its reactants. The H<sub>2</sub>O returns to the scrubber and the salts become paste. The segregation of salts from recirculated scrubbing liquor is so energy efficient that it is done with the differential temperature provided by seawater and engine exhaust. There is also a nominal need for electrical power to operate conventional pumps.



• The ClO<sub>2</sub> used in the gas/mist phase SO<sub>X</sub> or SO<sub>X</sub> and NO<sub>X</sub> scrubbing processes is the compound that selectively reacts with organic compounds including the polycyclic aromatic hydrocarbons (PAH) [1], [2] which become soot in marine exhaust gas stream. This is explained in greater detail in the body of this paper.

The exceptional  $SO_X$  and soot, or  $SO_X$  and  $NO_X$  and soot removal efficiency of the  $ClO_2$  based gas/mist phase scrubbing technology described herein is possible in large part because the process overcomes the solubility challenges of the target compounds in the exhaust gas. The process utilizes gas phase reactions to treat compounds that have low or no solubility in  $H_2O$ , for example nitrogen monoxide (NO) and PAH's. The mist phase of this process reacts with compounds that are soluble in water, for example  $SO_X$  and  $NO_2$ . The result is greater than >99.8% removal efficiency for  $SO_X$  and  $NO_X$  [3] and appreciable removal of PAH. The PAH removal efficiency varies with fuel type but is always less than the 50 ug/L IMO requirement for PAH's [4].

The ClO<sub>2</sub> based gas/mist scrubbing technologies ability to capture sulfur or nitrogen salts as separate pastes is another technological breakthrough. The proprietary process includes a closed loop that recycles an intermediary compound that promotes the precipitation of salts from scrubber liquor before they reach conventional saturation. If required, the paste can be dehydrated to granular powder with the addition of a conventional hot air spray dryer or similar technology.

#### 2 CLO<sub>2</sub> BASED GAS/MIST SCRUBBER CHEMISTRY

The same reaction chamber is used to selectively treat  $SO_X$  or  $SO_X$  and  $NO_X$  compounds. Differences in the reaction rates make this selective removal possible. The  $SO_X$  reactions can be summarized as described in eqns (1) and (2):

$$5 \text{ SO}_2 + 2 \text{ ClO}_2 + 6 \text{ H}_2\text{O} \rightarrow 5 \text{ H}_2\text{SO}_4 + 2 \text{ HCl},$$
 (1)

$$SO_2 + 2 NaOH \rightarrow Na_2SO_3 + H_2O.$$
 (2)

Chemical cost savings occur by utilizing the NaOH as described in eqn (2) as the first reactant with SO<sub>X</sub> and then introducing only as much ClO<sub>2</sub> according to eqn (1) as required to complete the SO<sub>X</sub> removal.

The ratio of NaOH to ClO<sub>2</sub> as well as the volume of both is regulated by multi sensor technology and process control logic (PCL) programs that optimizes chemical use. Inlet and exhaust gas SO<sub>X</sub> concentrations are compared along with reaction liquor pH and other variables in real time.

The  $NO_X$  reactions are summarized in eqns (3)–(5).

$$5 \text{ NO} + 2 \text{ ClO}_2 + \text{H}_2\text{O} \rightarrow 5 \text{ NO}_2 + 2 \text{ HCl},$$
 (3)

$$5 \text{ NO}_2 + \text{ClO}_2 + 3 \text{ H}_2\text{O} \rightarrow 5 \text{ HNO}_3 + \text{HCl}.$$
 (4)

There are differences in the rate of reaction between eqns (3) and (4). Eqn (3) is faster. The difference in reaction rates is adroitly utilized by additional sensor technology and PCL program logic to equalize the NO and NO<sub>2</sub> ratio in preparation for NO<sub>X</sub> abatement with the lower cost chemicals as described in proprietary eqn (5).

$$2 \text{ NaOH} + \text{NO}_2 + \text{NO} + (**) \rightarrow 2 \text{ NaNO}_2 + \text{H}_2\text{O},$$
 (5)

(\*\*) Options:

- $H_2O_2 = 85-90\%$  removal efficiency;
- $O_3 = 95\%$  removal efficiency;
- NaOCl = 90–95% removal efficiency;
- $Ca(OCl)_2 = 90-97\%$  removal efficiency.

$$2 \text{ NO}_2 + 2 \text{ NaOH} \rightarrow \text{NaNO}_2 + \text{NaNO}_3 + \text{H}_2\text{O}. \tag{6}$$

The compounds identified by \*\* enhance the eqn (5). They are provided to promote the reaction and are supplied in quantities that are a small percent of the NaOH. Eqn (5) includes several options for process promoters. The choices provide alternatives where a client or regulatory agency has an objection or preference.

The reaction with NaOH described in eqn (6) is presented because it occurs but at a much slower rate than eqn (5).

The process control logic allows eqns (5) and (6) to pre-treat the  $SO_X$  gas stream because they are less expensive, then  $ClO_2$  is added to the mist to achieve a removal efficiency of >99.8%  $SO_X$  that is not possible by eqns (5) and (6).

As noted, the chemical dosing in the  $ClO_2$  based gas/mist scrubbing system is regulated with sophisticated sensor/process control technology. However, the scrubbing technology includes a "polishing module" with chemistry that removes any unused  $ClO_2$ . The chemistry of this polishing module eqn (7) also contributes to removal of any stray  $SO_X$  or  $NO_X$  per eqns (8)–(10)

$$10 \text{ Na}_2\text{S}_2\text{O}_3 + 2 \text{ ClO}_2 + 4 \text{ H}_2\text{O} \rightarrow 2 \text{ NaCl} + 5 \text{ Na}_2\text{S}_4\text{O}_6 + 8 \text{ NaOH}.$$
 (7)

The sodium tetrathionate (Na<sub>2</sub>S<sub>4</sub>O<sub>6</sub>) formed in eqn (7) is reported on MSDS to not be a carcinogen. There is no reported environmental fate or toxicity.

The acids generated in eqns (1), (3) and (4) are removed according the eqns (8)–(10) shown below. Once again, the sensors and process control monitor the pH of the washwater and gas sensors monitor the target compounds in the gas stream to optimize chemical usage and ensure the exhaust gas and washwater quality are within IMO compliance

$$H_2SO_4 + 2 \text{ NaOH} \rightarrow \text{Na}_2SO_4 + 2 H_2O_7$$
 (8)

$$HCl + NaOH \rightarrow NaCl + H_2O,$$
 (9)

$$HNO_3 + NaOH \rightarrow NaNO_3 + H_2O.$$
 (10)

## 3 FORMATION OF MARINE SOOT

Literature teaches us that the formation of soot is a progressive process that occurs in the in the engine and exhaust ducting. It begins with smaller organic compounds, for example benzene, toluene, acetylene and 2–3 ring PAH's agglomerating. Large soot particles are formed when these "building blocks" combine to form molecules with mass between 500 and 1000 amu. ClO<sub>2</sub> has the ability to react with many of the organic soot precursor compounds and prevent them from agglomerating. Fig. 1 describes this reaction process between ClO<sub>2</sub> and phenanthrene (3 attached benzene rings) a challenging compound to scrub due to its very low solubility in water (1.6mg/L) and relative inertness in an ocean environment. Fig. 2 described the enhanced reactivity and solubility introduced into the parent phenanthrene by substitutions that result from the reaction with ClO<sub>2</sub>.

$$+ C1O_2 \longrightarrow -\begin{cases} 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{cases}$$

Figure 1: Examples of ClO<sub>2</sub> reactions with phenantherene [2].

Figure 2: Post ClO<sub>2</sub> reactions with phenantherene [2].

Fig. 3 is an excerpt from an article [5] in which the authors describe the soot formation process in detail. This figure elaborates on the summary provided in the previous paragraph.

"The molecular precursors of soot particles are thought to be heavy HAHs of molecular weight 500–1000 amu. The growth process from smaller molecules such as benzene to larger and larger PAH appears to involve both the addition of C<sub>2</sub>, C<sub>3</sub> or other small units, among which acetylene (C<sub>2</sub>H<sub>2</sub>) has received much attention, to PAH radicals, and reactions among the growing aromatic species, such as PAH–PAH radical recombination and addition reactions. In experimental studies, PAHs have been found to be the dominating compounds in the sooting zone of premixed flames as well as other combustion environments. The role of ions and fullerenes in soot formation is currently under discussion as well. Comprehensive reviews and literature regarding soot formation are available.

After the early work of Berthelot, who suggested the formation of benzene via direct polymerization of acetylene, and bone and Coward, who hypothesized a potential role for CH<sub>2</sub> and CH fragments, there are several possible reaction pathways leading to the first aromatic ring formation in the gas phase" [5].

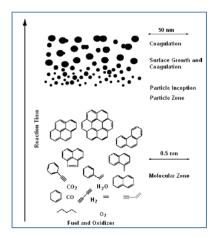


Figure 3: Formation of Molecular Precursors of Soot [5].

Example Reactions with PAH's are shown graphically in Figs 1 and 2. The equations reflect actual reaction products but the diagrams are not balanced.

Once the phenanthrene has reacted with ClO<sub>2</sub> the products with substitutions have enhanced reactivity and solubility. These reaction products undergo further decomposition in an ocean environment. Examples are shown in Fig. 2.

The important point is that this ClO<sub>2</sub> based gas/mist phase scrubbing technology reduces the formation of soot by reacting with a sufficient portion of the organic compounds that are precursors to large soot molecules. The efficiency of the ClO<sub>2</sub> reaction with organics varies with fuel types, but in all samples tested to date, the PAH concentration in washwater was less than half of the IMO's maximum 50ug/L concentration limit.

The  $ClO_2$  based gas/mist scrubbing process removes the soot precursor compounds in the same reaction chamber and at the same time it is reacting with  $SO_X$  or  $SO_X$  and  $NO_X$ . This process is sufficiently effective to allow discharge of the  $SO_X$  reaction products to be introduced directly into the sea without further treatment. This process has no need for the post scrubbing treatment of wastewater that is required when seawater is used to scrub  $SO_X$ .

As mentioned before, the high removal efficiency success of this  $ClO_2$  based gas/mist scrubbing technology is the result of an effective combination of gas and mist phase reactions. The gas phase has reaction advantages with compounds that are not soluble in water and the mist phase reactions are applicable to water soluble compounds. However, this is just a generality. The success is in the details. The narrative associated eqns (1)–(10) described complexities in mist combinations necessary for this process to achieve its exceptional removal efficiency.

## 4 CLO<sub>2</sub> BASED GAS/MIST SCRUBBING EQUIPMENT

Fig. 4 describes the general components of this scrubbing process. The graphic depicts the standalone option for this technology. The ClO<sub>2</sub> gas/mist scrubbing process is quite

adaptable, other design configurations are available. Furthermore, the reaction chamber can be oriented in any direction because it does not have a liquid scrubber sump. This ClO<sub>2</sub> based gas/mist scrubbing will not have any operational problems associated with dramatic changes in ship angle during a storm conditions. Such angular deviations would adversely affect a conventional seawater scrubber with liquid sump and packed bed design.

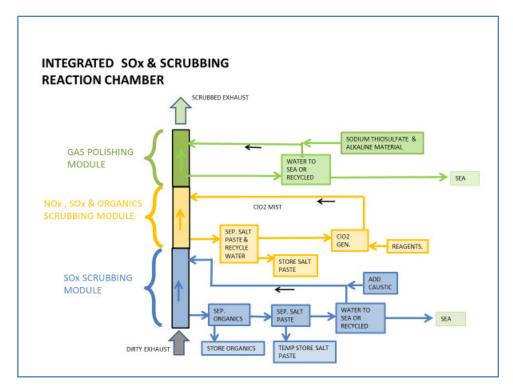


Figure 4: Process flow diagram for the ClO<sub>2</sub> based gas/mist scrubbing system.

#### 5 FIXED AND OPERATIONAL COSTS

The complexity of the equipment supplied by the ClO<sub>2</sub> based gas/mist scrubber is similar to the currently available seawater SO<sub>X</sub> scrubber technology. Equipment and installation costs are expected to be similar; however there is another variable that must be considered before an accurate value comparison is made.

None of the seawater based  $SO_X$  scrubbers are capable of treating  $NO_X$  when required by IMO and national rules. The  $ClO_2$  based gas/mist scrubber can treat both without any upgrades. The  $ClO_2$  based gas/mist scrubber is providing two scrubbers in the space of one and at the cost of one, and also eliminates a second loss of billable sailing time associated with a  $NO_X$  scrubber installation in the future.

#### 6 CONCLUSION

When compared to sea water  $SO_X$  scrubbing with its inability to effectively treat sludge from organic compounds and limitations associated with closed loop operation, the innovative  $ClO_2$  based gas /mist scrubbing of  $SO_X$ ,  $NO_X$  and organic compounds described in this paper is an intriguing alternative.



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