

Equivalence of two approaches to study the stress-strain relation in the myocardium

R. M. Shoucri

*Department of Mathematics and Computer Science,
Royal Military College of Canada, Kingston, Ontario, Canada*

Abstract

A method to study the mechanics of ventricular contraction was developed in previous publications by the author. In those studies, the active force of the myocardium is represented as force per unit volume of the myocardium. Other authors have developed studies in which the active force of the myocardium is included in the expression of the total stress derived from the constitutive relations. The purpose of the present study is to show how to make the connection between these two approaches. Derivation is done in a general way, expressions for the stress components are derived and application to experimental data is presented. The possibility of relating the pseudo strain energy function to the tension generated by the muscular fibre is also shown.

Keywords: cardiac mechanics, mathematical modelling of ventricular contraction, pressure-volume relation, active force of the myocardium, pseudo strain energy function.

1 Introduction

In previous studies by the author a method to study the stress-strain relation in the myocardium was developed in which the active force generated by the myocardium was represented as force per unit volume of the myocardium [1-6]. This mathematical approach used a cylindrical model of the left ventricle and was successfully developed by using both large elastic deformation [1, 2] and linear elasticity [3, 4], the transition from large elastic deformation to linear elasticity was discussed in [6]. Most other studies that have been developed focus on the way the expression of the total stress can be derived from the constitutive relations [9-11].



In this study the myocardium is represented as a thick-walled incompressible cylinder in which the myocardial fibres are imbedded in a helical way in a soft incompressible medium (see fig. 1). The contraction of the cylinder is modelled in a way to take into consideration torsion and shear, it turns out that their effect is small for the purpose of the numerical calculation of this study. In the quasi-static approximation used in this study, inertia forces and viscous forces are neglected. The total stress induced in the passive medium of the myocardium t_{ij} is written in the form $t_{ij} = \sigma_{ij} + q_{ij}$, where q_{ij} is the stress induced by the muscular fibre tension T and reflects the directional character of the stress; σ_{ij} is the stress resulting from the deformation of the passive medium of the myocardium (passive medium assumed isotropic). A similar approach can be found in Spencer [11]. Nevo and Lanir [8] have introduced a quantity similar to q_{ij} as the derivative of a hydrostatic pressure, and Arts et al. [12] have used an approach where σ_{ij} is replaced by a hydrostatic pressure.

The purpose of this study is to show the equivalence of the formalism developed in [1-6] by the author with the formalism developed by Humphrey and Yin [9] in which the total stress t_{ij} induced in the myocardium is derived from a pseudo strain energy function W . It is also shown how W can be directly related to the muscular fibre tension T , and that the splitting of $W = W_{iso} + W_{aniso}$ into an isotropic and an anisotropic component [9, 13, 14] is equivalent to the aforementioned splitting of the total stress t_{ij} .

2 Mathematical formalism: first approach

2.1 Equilibrium conditions

This is the approach used in [9, 10], in which the calculation is carried out by using the total stress t_{ij} . By assuming symmetry around the z-axis (solution independent of θ), the conditions of local equilibrium the myocardium ($\text{div } \mathbf{t} = 0$) can be written as follows in cylindrical coordinates

$$\frac{\partial t_{rr}}{\partial r} + \frac{t_{rr} - t_{\theta\theta}}{r} + \frac{\partial t_{zr}}{\partial z} = 0 \quad (1a)$$

$$\frac{1}{r^2} \frac{\partial(r^2 t_{r\theta})}{\partial r} + \frac{\partial t_{z\theta}}{\partial z} = 0 \quad (1b)$$

$$\frac{1}{r} \frac{\partial(rt_{rz})}{\partial r} + \frac{\partial t_{zz}}{\partial z} = 0 \quad (1c)$$

The stress can be dependent on the z variable, but we shall simplify the mathematical formalism by assuming that t_{zr} , $t_{z\theta}$ and t_{zz} are independent of z as in [9]. In this case eqns (1b) and (1c) give

$$r^2 t_{r\theta} = \text{const} = H_1 \quad r t_{rz} = \text{const} = H_2 \quad (2)$$

The radial stress boundary conditions on the surface of the cylinder are given by (see fig. 1).

$$t_{rr}(r_i) = -P_i \quad t_{rr}(r_o) = -P_o \quad (3)$$

2.2 Deformation gradient

The contraction of the myocardium is assumed to change the stress free configuration (R, Θ, Z) to the end-diastolic configuration $(r_{ed}, \theta_{ed}, z_{ed})$ and finally to (r, θ, z) during the systolic phase according to the relations

$$r_{ed} = r_{ed}(R), \quad \theta_{ed} = \alpha_1 \Theta, \quad z_{ed} = k_1 Z \quad (4)$$

$$r = r(r_{ed}), \quad \theta = \alpha_2 \theta_{ed} + \psi_2 z_{ed} + \chi(r_{ed}), \quad (5)$$

$$z = k_{2z} z_{ed} + k_{2\theta} \theta_{ed} + \omega(r_{ed})$$

which combined together give

$$r = r(R), \quad \theta = \alpha \Theta + \psi Z + \chi(R), \quad z = k_z Z + k_\theta \Theta + \omega(R) \quad (6)$$

The deformation gradient \mathbf{F}_I for the transformation from the stress free configuration (R, Θ, Z) to the end-diastolic configuration $(r_{ed}, \theta_{ed}, z_{ed})$ in cylindrical coordinates is given by [10]

$$\mathbf{F}_I = \begin{bmatrix} \frac{\partial r_{ed}}{\partial R} & \frac{1}{R} \frac{\partial r_{ed}}{\partial \Theta} & \frac{\partial r_{ed}}{\partial Z} \\ r_{ed} \frac{\partial \theta_{ed}}{\partial R} & \frac{r_{ed}}{R} \frac{\partial \theta_{ed}}{\partial \Theta} & r_{ed} \frac{\partial \theta_{ed}}{\partial Z} \\ \frac{\partial z_{ed}}{\partial R} & \frac{1}{R} \frac{\partial z_{ed}}{\partial \Theta} & \frac{\partial z_{ed}}{\partial Z} \end{bmatrix} = \begin{bmatrix} \frac{dr_{ed}}{dR} & 0 & 0 \\ 0 & \alpha_1 \frac{r_{ed}}{R} & 0 \\ 0 & 0 & k_1 \end{bmatrix} \quad (7)$$

The deformation gradient F_2 for the transformation from the end-diastolic configuration $(r_{ed}, \theta_{ed}, z_{ed})$ to the final configuration (r, θ, z) is given by

$$F_2 = \begin{bmatrix} \frac{\partial r}{\partial r_{ed}} & \frac{1}{r_{ed}} \frac{\partial r}{\partial \theta_{ed}} & \frac{\partial r}{\partial z_{ed}} \\ r \frac{\partial \theta}{\partial r_{ed}} & \frac{r}{r_{ed}} \frac{\partial \theta}{\partial \theta_{ed}} & r \frac{\partial \theta}{\partial z_{ed}} \\ \frac{\partial z}{\partial r_{ed}} & \frac{1}{r_{ed}} \frac{\partial z}{\partial \theta_{ed}} & \frac{\partial z}{\partial z_{ed}} \end{bmatrix} = \begin{bmatrix} \frac{dr}{dr_{ed}} & 0 & 0 \\ r \frac{d\chi}{dr_{ed}} & \alpha_2 \frac{r}{r_{ed}} & r\psi_2 \\ \frac{d\omega}{dr_{ed}} & \frac{k_{2\theta}}{r_{ed}} & k_{2z} \end{bmatrix} \quad (8)$$

The deformation gradient $F = F_2 F_1$ of the combined transformation is given by

$$F = \begin{bmatrix} \frac{\partial r}{\partial R} & \frac{1}{R} \frac{\partial r}{\partial \Theta} & \frac{\partial r}{\partial Z} \\ r \frac{\partial \theta}{\partial R} & \frac{r}{R} \frac{\partial \theta}{\partial \Theta} & r \frac{\partial \theta}{\partial Z} \\ \frac{\partial z}{\partial R} & \frac{1}{R} \frac{\partial z}{\partial \Theta} & \frac{\partial z}{\partial Z} \end{bmatrix} = \begin{bmatrix} \frac{dr}{dR} & 0 & 0 \\ r \frac{d\chi}{dR} & \alpha \frac{r}{R} & r\psi \\ \frac{d\omega}{dR} & \frac{k_\theta}{R} & k_z \end{bmatrix} \quad (9)$$

where $\alpha = \alpha_2 \alpha_1$, $\psi = \psi_2 k_1$, $k_\theta = k_{2\theta} \alpha_1$, $k_z = k_{2z} k_1$. By assuming that the transformations take place at constant volume, the incompressibility constraint can be written as follows

$$I_3 = (\det F)^2 = (\det F_2)^2 (\det F_1)^2 = 1 \quad (10)$$

where I_3 is the third strain invariant. By calculating the determinants in eqn (10) one obtains

$$\frac{dr}{dR} = \frac{R}{Kr}, \quad Kr^2 - R^2 = Kr_i^2 - R_i^2 \quad (11)$$

$$\frac{dr_{ed}}{dR} = \frac{R}{K_1 r_{ed}}, \quad K_1 r_{ed}^2 - R^2 = K_1 r_{ied}^2 - R_i^2 \quad (12)$$

$$\frac{dr}{dr_{ed}} = \frac{r_{ed}}{K_2 r}, \quad K_2 r^2 - r_{ed}^2 = K_2 r_i^2 - r_{ied}^2 \quad (13)$$

We have $K_1 = \alpha_1 k_1 = \det(F_1)$, $K_2 = \alpha_2 k_{2z} - \psi_2 k_{2\theta} = \det(F_2)$ and $K = K_1 K_2 = \det(F) = \alpha_1 k_1 \alpha_2 k_{2z} - \alpha_1 k_{2\theta} k_1 \psi_2 = \alpha k_z - k_\theta \psi$, with $\alpha = \alpha_1 \alpha_2$, $k_z = k_1 k_{2z}$, $\psi = \psi_2 k_1$, $k_\theta = \alpha_1 k_{2\theta}$. The inner radii are respectively R_i and r_i in the stress free configuration and during the systolic phase.

A muscular fibre in the myocardium is supposed to have a helical form on a cylindrical surface. In the undeformed configuration a unit vector \mathbf{N} with fibre angle $\Gamma(R)$ is transformed into a vector \mathbf{n} in the deformed configuration with fibre angle $\gamma(r)$ calculated with respect to the circumferential direction. With λ_N representing the stretch ratio in the direction of the muscular fibre, we have

$$\mathbf{n} = [0, \cos(\gamma(r)), \sin(\gamma(r))]^T, \quad \mathbf{N} = [0, \cos(\Gamma(R)), \sin(\Gamma(R))]^T \quad (14)$$

with

$$\mathbf{n} = \frac{1}{\lambda_N} \mathbf{F} \cdot \mathbf{N} \quad (15)$$

By using eqns (9) and (15) we get

$$\cos(\gamma(r)) = \frac{1}{\lambda_N} \left[\frac{\alpha r}{R} \cos(\Gamma(R)) + (r\psi) \sin(\Gamma(R)) \right] \quad (16)$$

$$\sin(\gamma(r)) = \frac{1}{\lambda_N} \left[\frac{k_\theta}{R} \cos(\Gamma(R)) + k_z \sin(\Gamma(R)) \right] \quad (17)$$

2.3 Constitutive relations

Relations between the components of the stress and deformation are known as constitutive relations. By assuming transverse isotropy with respect to the z-axis of the cylinder, Humphrey and Yin [9] have focused on a subclass of transverse isotropic material with pseudo strain energy function W given by the expression

$$W = W(I_1, \lambda_N) \quad (18)$$

where I_1 is the first strain invariant $I_1 = \text{tr}(\mathbf{B})$, and $\mathbf{B} = \mathbf{F} \cdot \mathbf{F}^T$ is the left Cauchy-Green deformation tensor. Written explicitly we have



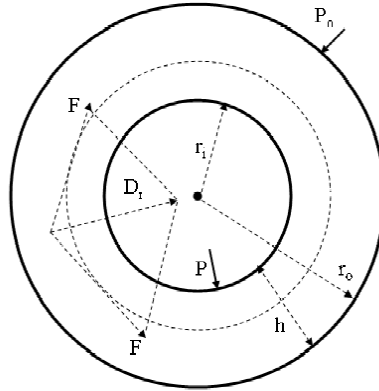


Figure 1: Cross-section of a cylinder representing the left ventricle. The dotted circle represents the projection of a helical fibre on the cross-section. $D_r(r)$ is the radial active force/unit volume of the myocardium. P_i is the ventricular pressure, P_o is the outer pressure, r_i is the inner radius, r_o is the outer radius, $h = b - a$ is the thickness of the myocardium.

$$B = \begin{bmatrix} \left(\frac{dr}{dR}\right)^2 & r \frac{dr}{dR} \frac{d\chi}{dR} & \frac{dr}{dR} \frac{d\omega}{dR} \\ r \frac{dr}{dR} \frac{d\chi}{dR} & \left(r \frac{d\chi}{dR}\right)^2 + \frac{\alpha^2 r^2}{R^2} + (r\psi)^2 & r \frac{d\chi}{dR} \frac{d\omega}{dR} + \frac{\alpha r k_\theta}{R^2} + r\psi k_z \\ \frac{dr}{dR} \frac{d\omega}{dR} & r \frac{d\chi}{dR} \frac{d\omega}{dR} + \frac{\alpha r k_\theta}{R^2} + r\psi k_z & \left(\frac{d\omega}{dR}\right)^2 + \frac{k_\theta^2}{R^2} + k_z^2 \end{bmatrix} \quad (19)$$

The Cauchy stress \mathbf{t} (force/current area) can be expressed by using eqn (18) in the form [9]

$$t_{ij} = -p\delta_{ij} + 2W_1 B_{ij} + W_{\lambda N} \lambda_N n_i n_j \quad (20)$$

where $W_1 = \frac{\partial W}{\partial I_1}$ and $W_{\lambda N} = \frac{\partial W}{\partial \lambda_N}$, p is a Lagrange multiplier introduced to

express the incompressibility condition for the myocardium. The first two terms in eqn (20) have an isotropic symmetry and the third term (the components of n_i are shown in eqn (14), part one) has a directional character corresponding to the

direction of the muscular fibre in the myocardium. We are now in a position to make the junction with the second approach developed in [1-6].

3 Mathematical formalism: second approach

3.1 Equilibrium conditions

We shall now see that it can be more instructive to work with the components σ_{ij} and q_{ij} of $t_{ij} = \sigma_{ij} + q_{ij}$. $T(r, z)$ is the stress in the direction of the muscular fibre in the myocardium. By assuming that a muscular fibre in the myocardium has a helical cylindrical shape as in the previous section, one can derive for the components of the stress q_{ij} the following relations as in [2, 15]

$$\begin{aligned} q_{rr} &= 0, & q_{\theta\theta} &= T(\cos \gamma(r))^2, & q_{zz} &= T(\sin \gamma(r))^2 \\ q_{z\theta} &= T \sin \gamma(r) \cos \gamma(r), & q_{r\theta} &= q_{rz} = 0 \end{aligned} \quad (21)$$

It is also possible to write the following relations

$$D_r = \frac{T}{r} (\cos \gamma(r))^2, \quad q_{z\theta} = r D_r \tan \gamma, \quad q_{zz} = r D_r \tan^2 \gamma \quad (22)$$

where D_r is obtained by substituting $t_{ij} = \sigma_{ij} + q_{ij}$ in eqns (1) and by writing the terms containing q_{ij} in the following way

$$D_r = \frac{q_{\theta\theta}}{r}, \quad D_\theta = -\frac{\partial q_{z\theta}}{\partial z}, \quad D_z = -\frac{\partial q_{zz}}{\partial z} \quad (23)$$

The quantities D_r , D_θ and D_z have the units of force/unit volume of the myocardium expressed in the three orthogonal directions of a cylindrical coordinate system. By using this notation, eqns (1) can be written in the form

$$\frac{\partial \sigma_{rr}}{\partial r} + \frac{\sigma_{rr} - \sigma_{\theta\theta}}{r} + \frac{\partial \sigma_{zr}}{\partial z} - D_r = \frac{\partial \sigma_{rr}}{\partial r} + \frac{\sigma_{rr} - \sigma_{\theta\theta}}{r} + \frac{\partial}{\partial z} (\sigma_{zr} - \int_z D_r dz) \quad (24a)$$

$$\frac{1}{r^2} \frac{\partial (r^2 \sigma_{r\theta})}{\partial r} + \frac{\partial \sigma_{z\theta}}{\partial z} - D_\theta = \frac{1}{r^2} \frac{\partial (r^2 \sigma_{r\theta})}{\partial r} + \frac{\partial}{\partial z} (\sigma_{z\theta} - \int_z D_\theta dz) \quad (24b)$$

$$\frac{1}{r} \frac{\partial (r \sigma_{rz})}{\partial r} + \frac{\partial \sigma_{zz}}{\partial z} - D_z = \frac{1}{r} \frac{\partial (r \sigma_{rz})}{\partial r} + \frac{\partial}{\partial z} (\sigma_{zz} - \int_z D_z dz) \quad (24c)$$

Because $t_{r\theta} = \sigma_{r\theta} (q_{r\theta} = 0)$ and $t_{rz} = \sigma_{rz} (q_{rz} = 0)$ we can write in a way similar to eqns (2)

$$r^2 \sigma_{r\theta} = \text{const} = H_1 \quad r \sigma_{rz} = \text{const} = H_2 \quad (25)$$

We assume that no external moment is applied to the myocardium, consequently the moment of forces M around the z-axis is zero

$$M = 2\pi \int_{ri}^{ro} (\sigma_{z\theta} + q_{z\theta}) r^2 dr = 0 \quad (26)$$

which gives

$$\sigma_{z\theta} = -q_{z\theta} \quad (27)$$

Equilibrium of forces in the longitudinal direction gives

$$\sigma_{zz} + q_{zz} + \tau_{av} = 0 \quad (28)$$

where τ_{av} is the average traction on the cross-section and is given by [8]

$$\tau_{av} = \frac{P_i r_i^2 - P_o r_o^2}{r_o^2 - r_i^2} \quad (29)$$

It is assumed that the average stress τ_{av} is independent of r and z .

3.2 Constitutive relations

It is assumed that the muscular fibre tension $T(r, z)$, and consequently q_{ij} , is uniformly distributed throughout the myocardium. By writing $t_{ij} = \sigma_{ij} + q_{ij}$ and by comparing eqns (21) with the last term of eqn (20) we can write

$$q_{ij} = W_{\lambda N} \lambda_N n_i n_j \quad (30)$$

with $W_{\lambda N}$ appropriately chosen such that

$$T = W_{\lambda N} \lambda_N \quad (31)$$

From eqn (20), the stress σ_{ij} can be expressed as follows

$$\sigma_{ij} = -p \delta_{ij} + 2W_1 B_{ij} \quad (32)$$



This last equation can be written with the help of eqn (19) in explicit form as follows

$$\sigma_{r\theta} = 2W_1 r \frac{dr}{dR} \frac{d\chi}{dR} = \frac{H_1}{r^2} \quad (33)$$

$$\sigma_{rz} = 2W_1 \frac{dr}{dR} \frac{d\omega}{dR} = \frac{H_2}{r} \quad (34)$$

$$\sigma_{z\theta} = 2W_1 \left[r \frac{d\chi}{dr} \frac{d\omega}{dR} + \frac{\alpha r k_\theta}{R^2} + r \psi k_z \right] \quad (35)$$

$$\sigma_{zz} = -p + 2W_1 \left[\left(\frac{d\omega}{dr} \right)^2 + \frac{k_\theta^2}{R^2} + k_z^2 \right] \quad (36)$$

$$\sigma_{\theta\theta} = -p + 2W_1 \left[\left(r \frac{d\chi}{dr} \right)^2 + \left(\frac{\alpha r}{R} \right)^2 + (r \psi)^2 \right] \quad (37)$$

$$\sigma_{rr} = -p + 2W_1 \left(\frac{dr}{dR} \right)^2 = -p + 2W_1 \left(\frac{R}{Kr} \right)^2 \quad (38)$$

These equations are used in the experimental application described in what follows. The term D_r appearing in eqn (24a) is similar, but not identical, to the introduction of a derivative of a hydrostatic pressure in eqn (26) of [8].

4 Application and results

The fibre angle $\gamma(r)$ (referred to the circumferential direction) is supposed to be constant with respect to the axial and circumferential directions. The radial variation of the fibre angle is supposed to be linear and given by

$$\gamma = \gamma_{end} \left(\frac{r_o - r}{r_o - r_i} \right) + \gamma_{epi} \left(\frac{r - r_i}{r_o - r_i} \right) \quad (39)$$

where $\gamma_{end} = 45^\circ$ is the fibre angle at the endocardium, and $\gamma_{epi} = -45^\circ$ is the fibre angle at the epicardium. The dimensions of the left ventricle in the diastolic configuration are outer radius $r_o = 3.38$ cm, inner radius $r_i = 1.02$ cm and length $\ell = 3.06$ cm as taken from experiment on dog reported in Feit [7]. The corresponding radii in the reference stress free configuration were estimated from eqn (11), part two, as $R_o = 3.4474$ cm and $R_i = 1.1$ cm. The tension T developed by the muscular by the fibre near the end-diastolic phase is taken from fig. 7a of Feit [7] and is reproduced in fig. 2 (left) of this study, fig. 2 (right)



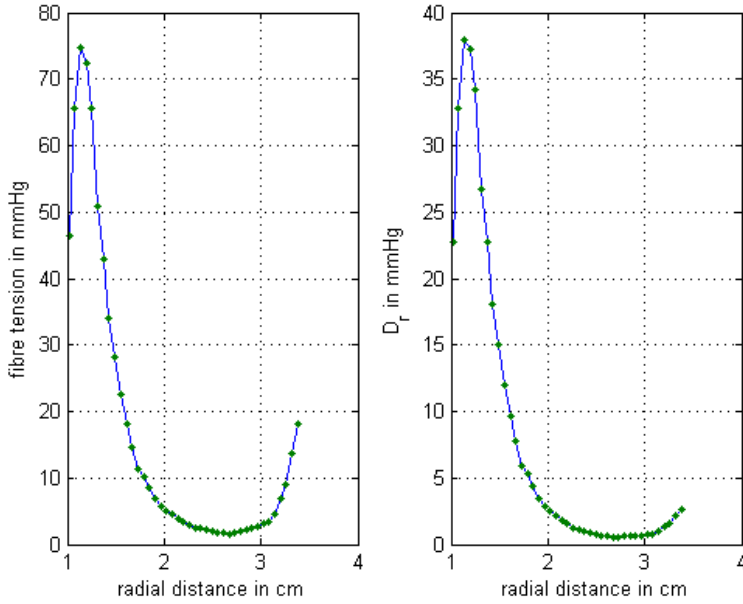


Figure 2: Radial variation from endocardium to epicardium of the fibre tension T reproduced from [7] (left), and of the radial active force/unit volume of the myocardium D_r (right).

shows the variation of D_r calculated from eqn (22), part one and (39). Similarly the active stress components $q_{z\theta}$ and q_{zz} are calculated respectively from eqn (22), parts two and three, $\sigma_{z\theta}$ and σ_{zz} are calculated respectively from eqns (27) and (28) and shown in fig. 3. We took the ventricular pressure $P_i = 10$ mmHg and the epicardial pressure $P_o = 0$ mmHg in the calculation of τ_{av} from eqn (29). The two quantities $d\chi/dr$ and $d\omega/dR$ are small and have been neglected in the calculation that follows. Consequently from eqns (35) – (38) one can derive the following equation to calculate σ_{rr}

$$\frac{\sigma_{z\theta}}{\sigma_{zz} - \sigma_{rr}} = \frac{(k_{\theta}\alpha r)/R^2 + k_z\psi r}{k_{\theta}^2/R^2 + k_z^2 - R^2/(Kr)^2} \quad (40)$$

and the following equation to calculate $\sigma_{\theta\theta}$

$$\frac{\sigma_{z\theta}}{\sigma_{\theta\theta} - \sigma_{rr}} = \frac{(k_{\theta}\alpha r)/R^2 + k_z\psi r}{(\alpha r)^2/R^2 + (\psi r)^2 - R^2/(Kr)^2} \quad (41)$$

The radial variation of σ_{rr} and $\sigma_{\theta\theta}$ is shown respectively in the left and right side of fig. 4.

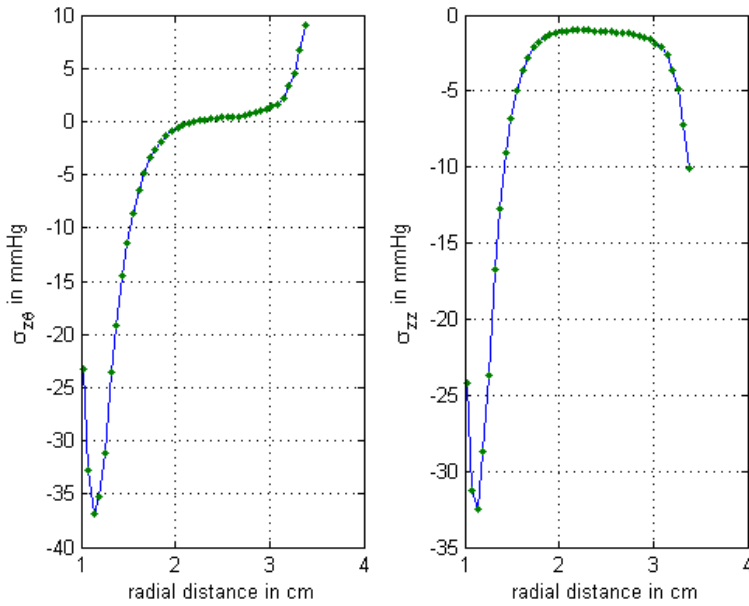


Figure 3: Radial variation from endocardium to epicardium of the stress $\sigma_{z\theta}$ (left), and of the axial stress σ_{zz} (right).

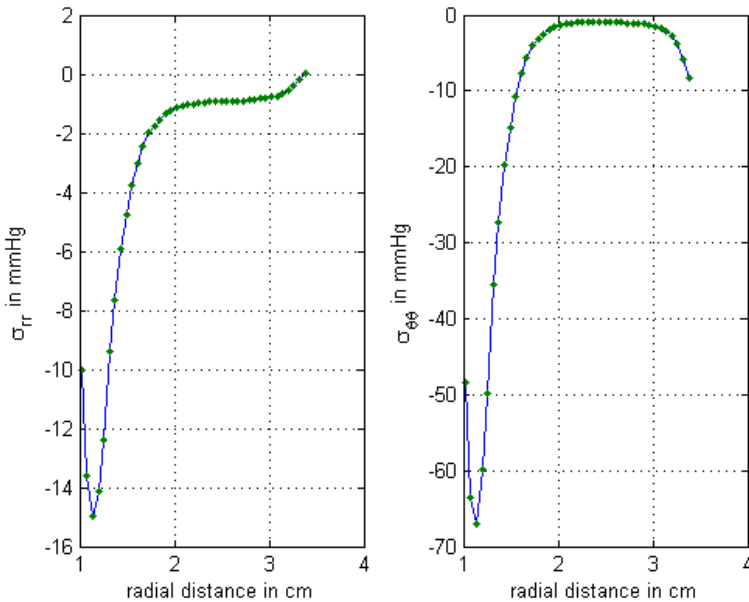


Figure 4: Radial variation from endocardium to epicardium of the radial stress σ_{rr} (left), and of the circumferential stress $\sigma_{\theta\theta}$ (right).



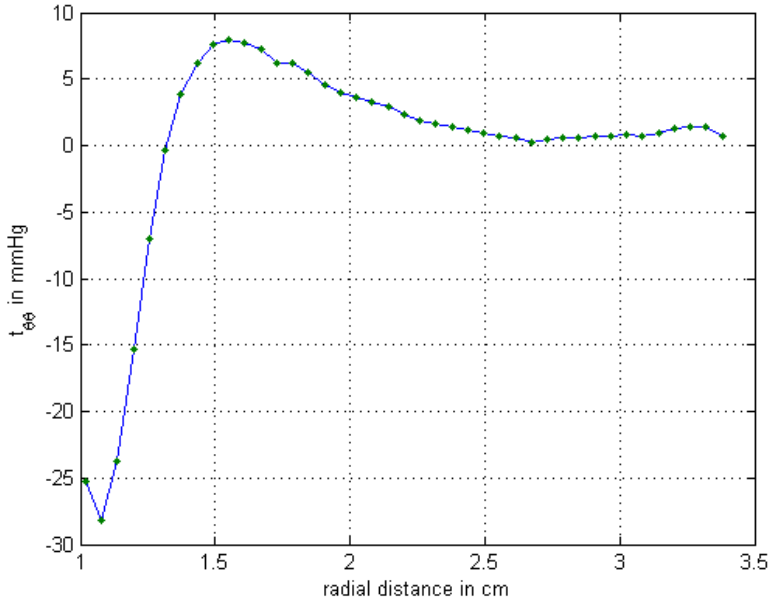


Figure 5: Radial variation of the total circumferential stress $t_{\theta\theta}$ from endocardium to epicardium.

In the calculation of σ_{rr} and $\sigma_{\theta\theta}$ we have made use of the two following conditions, first the incompressibility condition

$$\alpha k_z - \psi k_\theta = K \quad (42)$$

The second condition is that numerator of eqn (41) for $\sigma_{z\theta}$ is zero for $r_{zero} = 2.2$ cm from fig. 3 ($R_{zero}^2 = 5.1160$ from eqn (11), part two), which gives

$$\alpha k_\theta + \psi k_z R_{zero}^2 = 0 \quad (43)$$

Eqns (42) and (43) are solved to express α and ψ in terms of k_z and k_θ as follows

$$\psi = -\frac{k_\theta K}{k_\theta^2 + k_z^2 R_{zero}^2} \quad (44)$$

$$\alpha = \frac{k_z K R_{zero}^2}{k_\theta^2 + k_z^2 R_{zero}^2} \quad (45)$$

These values of ψ and α are substituted into eqn (40) evaluated at r_i ($\sigma_{rr} = -P_i = 10$ mmHg) and at r_o ($\sigma_{rr} = -P_o = 0$) with σ_{zz} calculated from eqn (28). The two equations obtained in this way are solved by using the Newton iteration

algorithm to calculate the two roots k_θ and k_z of a system of two coupled equations. For $r_i = 1.02$ cm, $r_o = 3.38$ cm, $K = 1.028$, $R_i = 1.1$ cm, $R_o = 3.4474$ cm, we have calculated $k_\theta = -0.1472$, $k_z = 1.0043$, eqns (44) and (45) give $\alpha = 1.0228$ and $\psi = 0.0057$. These are the values used to calculate the results of fig. 4.

From the results shown in figs 3 to 6, the radial variation of each of the stress components appears to be similar to that reported in ref. [9] with a difference of sign probably due to the fact that we use the convention that a negative stress represents compression, a positive stress represents tension. It is also important to note the difference between the stress components σ_{ij} and t_{ij} as is clear for instance by comparing fig. 4 (right) and fig. 5, and also how the three quantities W_I , $W_{\lambda N}$ and D_r can be expressed directly in terms of the muscular fibre T .

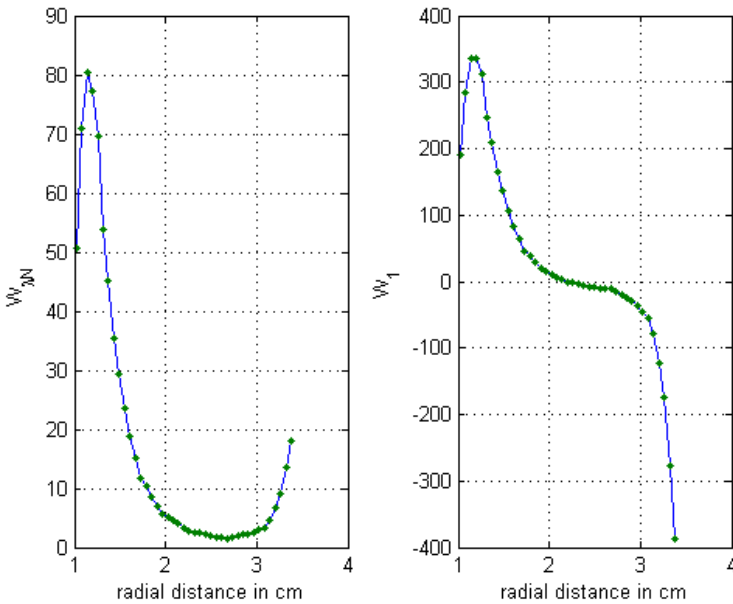


Figure 6: Radial variation from endocardium to epicardium of $W_{\lambda N}$ (eqn (31)) (left), and of W_I (eqn (38)) (right).

5 Conclusion

By introducing the concept of radial active force/unit volume of the myocardium, we have shown that it is possible to calculate the stress induced in the passive medium of the myocardium and the components of the active stress generated by the muscular fibre. One should note that all the calculations have been carried out without having to assume a model for the pseudo strain energy function; instead knowledge of the muscular fibre stress generated in the direction of the muscular fibre was necessary for our calculation. It is also

evident that the trend in the literature to split the pseudo strain energy function into an isotropic and a directional component is equivalent to the splitting of the total stress into two components as explained in this study.

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