Development of green composites using agricultural waste

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Abstract

This study deals with the development and evaluation of environment-friendly composites that are composed of polylactic acid (PLA) resin and rice straw. The rice straw fibers were extracted from rice straw harvested in Toyama city. The preliminary composites were prepared by mixed rice straw fiber and PLA resin, followed by drying at 50°C for 24 hours. Rice straw green composites were fabricated by the vacuum assisted hot pressing method. The mould temperature was changed from 150°C to 210°C, in order to investigate the effect of molding conditions on the mechanical properties of rice straw green composites. The molding pressure and time was fixed to 2 MPa and 10 minutes, respectively. The water evaporation rate for rice straw green composites was measured in order to investigate the variation in moisture with respect to the drying time for rice straw fiber or rice straw/PLA composites. The evaporation rate of rice straw/PLA composites was lower than that of rice straw fiber. The flexural strength and modulus increased with increasing fiber weight fraction of rice straw green composites; a peak flexural strength and a peak flexural modulus was reached at molding temperature ranges near 180°C and a fiber weight fraction of 30 wt.%.

Keywords: green composites, rice straw, polylactic acid, vacuum assisted hot press molding, flexural properties.

1 Introduction

In recent years, natural fiber reinforced thermoplastics (NF RTP) have been gaining considerable attention for their potential contribution to addressing environmental issues, such as reduction of carbon dioxide emissions and the saving of fossil resources. NF RTP have also attracted interest and have been

accepted widely into industrial fields, because of their high strength and stiffness, low cost and desirable recycling features [1–3]. The composite industry looks into alternative low cost lignocellulosic sources, which can decrease overall manufacturing costs and increase stiffness of the materials.

Rice straw is one of such major agricultural by-products, which contain cellulose, hemicellulose, lignin, silica and ash. Rice straw is an annually renewable fiber. According to the MAFF, Japan produced 8.5 million tons of rice in 2010 [4]. Most of rice straws are used as livestock feeding and plowing-in. Some rice straws are burned. However, rice straw may not be burned in many prefectures in Japan, because of environment regulation. Use of rice straw and other agricultural by-products as reinforcement in the production of composite materials alleviate the shortage of wood resource. Over past several years, there has been increasing interest in the use of rice straw and wheat straw as a reinforcing filler of wood-plastic composites. Thus, extensive research utilizing wheat straw and rice straw as filler for petroleum-based plastics, such as novolac resin, high-density polyethylene, low-density polyethylene, poly-vinyl alcohol and polypropylene, has been conducted [5–10]. Patil *et al.* [5] have manufactured a composite material composed of wheat straw filler and polypropylene, and reported their improved mechanical properties. Panthapulakkai and Sain [7] reported that wheat straw filled high-density polyethylene (HDPE) exhibited superior mechanical properties compared to cornstalk, corncob and even wood flour filled HDPE.

In this study, composites consisting of poly lactic acid (PLA) resin and rice straw fibers have been prepared by a vacuum assisted hot pressing method. Rice straw fibers were extracted from rice straws after rice harvest. The mechanical properties of rice straw fiber and PLA matrix have been examined from a viewpoint of determining the optimum molding condition of vacuum assisted hot pressing. The effect of molding conditions on the mechanical properties of rice straw green composites has also been investigated.

2 Experimental procedure

2.1 Materials

The matrix polymer used is polylactic acid (PLA, LANDY PL-1000, Miyoshi Oil & Fat Co., Ltd., Japan). The rice straw fibers were extracted from rice straws harvested in Toyama city. To extract the rice straw fibers, the rice straw was immersed for 3 hours in a solution of NaOH with 5 mol/l concentration at 90°C. The rice straw fibers were washed in pure water to remove the impurities that remained on their surface. Then, they were dried at 50°C for at least 24 hours in order to reduce the effect of the water content of consolidation behavior. Figure 1 shows the appearance and the SEM image of the rice straw fiber.

Figure 1: Rice straw fiber.

2.2 Preparation of preliminary composites

In order to facilitate the molding of green composites with a hot pressing machine, the preliminary composites were prepared by mixed rice straw fiber and PLA resin using a non-bubbling kneader (NBK-1, Nihonseiki Kaisha, Ltd., Japan), followed by drying at 50°C for 24 hours using a drying oven (EPN-115, Isuzu Seisakusho Co., Ltd., Japan). Figure 2 shows a finished preliminary composite material.

Figure 2: Photograph of preliminary composite.

2.3 Hot pressing of rice straw green composites

Fig. 3 shows the schematic view of the vacuum assisted hot press molding. The vacuum assisted hot press molding was carried out using a hot pressing machine (AH-2003, As one Co., Ltd., Japan) and a vacuum pump, after setting the preliminary composites in a metallic mould, then covering a mould with the vacuum bag. The molding temperature was changed from 150°C to 210°C. The molding pressure and time was fixed to 2 MPa and 10 minutes, respectively.

2.4 Flexural testing

In order to evaluate the mechanical properties of rice straw green composites, the 3-point flexural test was carried out using a universal testing machine (Ez-graph, Shimadzu Co. Ltd., Japan) at room temperature. The dimensions of the specimen are 15 mm width, 60 mm length and 2 mm thickness, respectively. The flexural test was performed under the follow conditions: cross-head speed of 1.0 mm/min and span length of 40 mm.

Figure 3: Schematic view of vacuum assisted hot press molding.

2.5 Water evaporation rate

Measurement of the water evaporation rate for rice straw green composites was carried out using a moisture analyzer (MOC63u, Shimadzu Co. Ltd., Japan). The temperature and time were set at 100°C and 1 hour, respectively. The water evaporation rate R is given by the following equation:

$$R = \frac{M_W - M_D}{M_W} \times 100 \quad (1)$$

where M_W is the mass of undried material when measurement starts, M_D is the mass of dried materials when measurement ends.

3 Results and discussion

3.1 Water evaporation rate

Fig. 4 shows the variation in the water evaporation rate with respect to the drying time for rice straw fiber and rice straw/PLA composites. The water evaporation curves of both materials showed similar behavior; the moisture evaporated rapidly during the first stages (0–200 s) reaching a certain value, the saturation point, at which no more moisture was evaporated and the content of moisture in the materials remained the same. The evaporation rate of rice straw/PLA composites is lower than that of rice straw fiber because the particles of PLA resin adhere to the rice straw fibers by mixing PLA resin with the rice straw fibers and drying the composites.

3.2 The effect of fiber weight fraction on flexural properties

Fig. 5 shows the results of flexural tests for rice straw green composites molded at 2 MPa and 150°C. The flexural strength increases with increasing the fiber weight fraction, and indicates a peak flexural strength of 83 MPa at a fiber weight fraction of nearly 30 wt.%. The maximum flexural strength

Figure 4: Evaporation rate of rice straw and rice straw/PLA.

Figure 5: Relationship between flexural strength, flexural modulus of rice straw green composites and fiber weight fraction.

corresponds to 1.3 times the strength of PLA resin. It is proven that the flexural modulus also shows a similar dependence with increasing the fiber weight fraction. The maximum flexural modulus corresponds to 1.4 times the flexural modulus of PLA resin. However, the composites with a high content of rice straw fibers (over 30% by weight) showed lower flexural strength than that without the addition. Fig. 6 shows SEM images of the fracture surface of rice straw green composites specimens as a result of the flexural test. Extensive debonding, clean rice straw fibers and some voids, indicating the poor

fiber/matrix adhesion, can be found in all the specimens. The observation result suggests that the poorer stress transfer at fiber/matrix interface caused the decrease in strength of the composites. As the reasons for the deterioration of interfacial adhesion, it is suggested that the PLA matrix did not fully permeate to the inside of rice straw green composites due to the high viscosity of PLA matrix and the poor wettability on the fiber surface. Moreover, the rice straw fibers contain moisture, because the preliminary composites were fabricated by kneading rice straw fiber and water-dispersion type PLA resin. Then, although the preliminary composites were fully dried, moisture has been included in the preliminary composites. The moisture contained in preliminary composites or rice straw evaporates by the heating of hot pressing. Therefore, it is supposed that the steam made damage easy to occur in fiber/matrix interfaces by applying pressure to the resin surrounding a fiber, and that hydrolysis of PLA matrix in the vicinity of the rice straw fibers occurred by reaction with the moisture, which remained in rice straw fibers or preliminary composites during the course of heating.

Figure 6: SEM images of fracture surface of rice straw green composites. (Molding temperature 150°C.)

3.3 The effect of heat treatment on mechanical properties of fiber, matrix

In order to establish the most suitable molding conditions, the mechanical properties of rice straw fiber and PLA matrix were determined. Fig. 7 shows the Weibull plots for the tensile strength of rice straw fibers with varying

temperature. The Weibull shape and scale parameters as well as mean, standard deviation and correlation coefficient computed from these Weibull distributions are listed in table 1. The average tensile strength of rice straw fibers heat-treated at 150°C is 136.2 MPa. The tensile strength of rice straw fibers heat-treated at 180°C is similar to that of rice straw fibers heat-treated at 150°C. However, the tensile strength of rice straw fibers heat-treated at 210°C markedly decreases as compared with that of rice straw fibers heat-treated at 180°C. The tensile strength drops by about 30%, from 142.8 MPa down to 98.0 MPa. Fig. 8 shows the effect of molding temperature on the flexural properties of PLA matrix.

Table 1: Weibull parameters and factors of tensile strength of rice straw fibers with the various treated temperatures.

Treated temperature (°C)	Shape parameter α	Scale parameter σ_0	Mean μ	Standard deviation SD	Correlation coefficient R
150	3.11	152.2	136.2	47.3	0.989
180	4.24	157.0	142.8	37.3	0.975
210	2.59	110.4	98.0	40.4	0.954

Figure 7: Weibull distribution plots for tensile strength of rice straw fiber with varying temperature.

It is obvious that the flexural modulus does not decrease even with higher molding temperature, while the flexural strength indicates a peak flexural strength of 48.5 MPa at a molding temperature range of about 180°C and decreases with the rise of molding temperature above 180°C. Based on these results, the processing temperature for molding rice straw green composites should be kept below 180°C in order to prevent strength reduction due to thermal degradation.

Figure 8: Relationship between flexural strength, flexural modulus of PLA and molding temperature.

3.4 The effect of molding temperature on flexural properties

Fig. 9 describes the change of flexural properties with the molding temperature. The flexural strength and the flexural modulus of rice straw green composites indicate a peak value at a molding temperature range of about 180°C. The flexural strength and the flexural modulus of rice straw composites molded at 180°C are approximately 94 MPa and 5 GPa, respectively, which are 12% higher than those at 150°C. However, the green composites with a high molding temperature above 180°C showed lower flexural strength and modulus than that with a molding temperature at 180°C. Fig. 10 shows SEM images of the fracture surface of rice straw green composites, which contain 30 wt.% rice straw fiber. The adhesion between the rice straw and PLA matrix in the rice straw green composites molded at 180°C seems to be better than that molded at 150°C, and the rice straw fibers are imbedded in the PLA matrix, which indicates good wetting by the polymer. The rise of molding temperature can be effective in improving the mechanical properties of rice straw green composites, because the viscosity of PLA matrix becomes lower, and the PLA matrix fully permeates to the inside of rice straw green composites. However, the fracture surface of rice straw green composites molded at 210°C seems to be rough. This observation result suggests that the rise of molding temperature caused the decrease in strength of the composites due to thermal degradation as discussed in section 3.3. In addition, debonding or clean rice straw fibers can be found in all the green composites. It is proven that the bonding between rice straw fiber and PLA matrix was not thus improved even if the green composites were molded under the optimum condition.

Figure 9: Relationship between flexural strength, flexural modulus of rice straw green composites and molding temperature.

Figure 10: SEM images of fracture surface of rice straw green composites. (Fiber weight fraction 30wt.%.)

4 Conclusions

The mechanical properties of rice straw green composites fabricated by a vacuum assisted hot press molding have been investigated. Summarized results and remarks are as follows.

- 1) The water evaporation curves of both materials showed similar behavior. The evaporation rate of rice straw/PLA composites is lower than that of rice straw fiber.
- 2) The flexural strength increases with increasing the fiber weight fraction, and indicates a peak value at a fiber weight fraction of nearly 30 wt.%.
- 3) The optimum molding temperature is 180°C among the conditions investigated.

- 4) The flexural strength and flexural modulus obtained are approximately 94 MPa and 5 GPa, respectively. This flexural strength is 12% higher than that of rice straw green composites molded at 150°C.

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